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ADDENDUM TO MUNGLINUP DFS RESULTS ANNOUNCEMENT

Mineral Commodities Ltd ("MRC" or "the Company") provides the following information as an addendum to the ASX release issued on 8 January 2020 entitled "ROBUST MUNGLINUP DFS RESULTS ALLOW MRC TO MOVE TO 90% OWNERSHIP OF MUNGLINUP GRAPHITE PROJECT". References to page numbers relate to the aforementioned ASX release.

Mineral Resource and Reserve - Page 3

Pursuant to ASX Listing Rule 5.9.1, and in addition to the information contained in the body of the release issued on 8 January 2020, MRC provides the following summary information:

- The Ore Reserves are based on key modifying factors that include optimisations, analyses, detailed designs, schedules and cost estimates of a Definitive Feasibility Study that describes development of the project to produce up to 69,800tpa of graphite concentrate for approximately 14 years at an average production rate of 52kt per year.
- Metallurgical testwork has been completed by ALS Metallurgy (and a small number of potential equipment suppliers to gauge equipment appropriateness) and supervised by BatteryLimits or Orway Mineral Consultants. The work undertaken by these reputable and experienced specialists is described in this document and supports the related modifying factors applying to the Ore Reserve estimate.
- The mining schedule has been estimated on Indicated and Inferred Mineral Resources reported in accordance with the JORC Code (2012 edition) with detailed mine designs, specifications from geotechnical studies and mining equipment determined by experienced engineers and mining contractors. Indicated material is generally classified as being where the nominal drill hole spacing is 40m or less, while drilling wider than 40m spaced sections and down dip extensions between 20-50m down dip of the current drilling were classified as Inferred.
- The mining method selected for the Munglinup Graphite Project is open pit mining applying conventional truck and excavator techniques. This method is commonly practised in this style of deposit and region. Given the high grade mineralisation, general lack of requirement for drill and blast activities, and small excavators being employed, a mining recovery factor of 98% and dilution factor of 5% have been applied. The weathered nature of the ore material, along with the potential to be upgraded significantly, has resulted in there being no significant deleterious elements in the production of concentrate.
- The processing flowsheet is based on metallurgical testwork undertaken using composites that are representative of the deposit in terms of material type, grades and spatial distribution. Overall, the proposed process plant facilities for the Munglinup

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Graphite Project in the Definitive Feasibility Study ("DFS") comprise processes and equipment that are aligned with similar operations.

- The processing plant has been developed by experienced process design engineers, BatteryLimits and Mondium, and is presented to an appropriate level of design required to support the recovery, throughput and production estimates set out in the DFS.
- The infrastructure requirements, including the Tailings Storage Facility ("TSF"), have been designed and defined by specialist engineers and appropriately experienced industry consultants.
- The detailed designs discussed above have been used as the basis for capital and operating cost estimates derived from first principles estimates, benchmark data, scaling of comparable design components and vendor quotes.
- The determination of ore and waste was calculated using a cash flow script that considers, on a block by block basis, graphite recovery, estimated flake size distribution and operational costs including mining, processing and logistics.
- The basis for quality parameters applied to the Ore Reserve are fundamentally metallurgical testwork and research into the desirability of the Munglinup graphite product in the current and emerging markets for graphite products and application in further downstream processing.
- The status of approvals, tenements and licences are as follows:
  - The Munglinup Graphite Project is located within a granted Mining Lease.
  - The mining, environmental and social permitting process is well underway with the Mining Proposal, Mine Closure Plan, Works Approval application, Prescribed Premises Licence application, and Dangerous Goods licence application scheduled to be submitted following the grant of environmental approvals, which are currently under review by the Western Australian Environmental Protection Agency and the Federal Department of the Environment and Energy under an accredited process.
- Graphite concentrate produced at Munglinup is currently proposed to be trucked to the Fremantle Port and shipped to various international ports as required.

Cautionary Statements – Page 4

The DFS discussed herein has been undertaken to determine the feasibility to mine and process graphite ore from a production plant constructed at Munglinup. The DFS is predicated on a Pre-Feasibility Study ("PFS") (see ASX announcement dated 30 May 2018) completed in May 2018 and is based on the same project sizing as developed during the PFS. The DFS is a continued technical and economic study of the PFS considering the development of the Munglinup Graphite Deposit and builds on the mine design and engineering assessment described in the PFS. The operating parameters of the DFS differ materially from the plan and assessments described in the PFS and are based on feasibility-level technical and economic assessments. The DFS evaluation work and appropriate studies have provided feasibility-level

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estimates of cost and rates of return to provide an assurance of an economic development based on the DFS.

The production targets underpinning financial forecasts included in the DFS include 61% Indicated Resources and 39% Inferred Resources over the 14 year mine life. No exploration target material has been included in the economic valuation or production target of Munglinup. There is a lower level of geological confidence associated with Inferred Mineral Resources and there is no certainty that further exploration work will result in the determination of additional Indicated Mineral Resources or that the Inferred Mineral Resources will add to the economics of Munglinup. However, in preparation of the production target and associated NPV, each of the modifying factors were considered and have therefore passed the "economics test".

The DFS is based on the material assumptions outlined elsewhere in this announcement. These include assumptions about the availability of funding.

MRC considers all of the material assumptions to be based on reasonable grounds. To achieve the range of outcomes indicated in the DFS, additional funding will likely be required. Investors should note that there is no certainty that MRC will be able to raise the amount of funding required. It is also possible that such funding may only be available on terms that may be dilutive to or otherwise affect the value of MRC's existing shares. It is also possible that MRC could pursue other "value realisation" strategies such as a sale, partial sale or additional joint venture partners of Munglinup. If it does, this could materially reduce MRC's proportionate ownership of Munglinup.

Funding – Page 11 (Page 5 of presentation)

Preference for ring-fenced, limited/non-recourse project debt finance as opposed to a more general corporate debt finance.

Capital Cost – Page 15 (Page 9 of presentation)

The capital requirement for increasing throughput of the circuit to 500ktpa in 2027 is included in the sustaining capital estimate (refer to the JORC Code (2012) Table 1 which is attached for additional information).

Operating Costs – Page 16 (Page 10 of presentation)

The operating cost estimate has been prepared to an accuracy of +15/-5% by independent experts. This includes labour numbers, estimated salaries, maintenance costs, consumables

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required at the plant, diesel burn rates and plant power draw requirements (refer to the JORC Code (2012) Table 1 which is attached for additional information).

Industry standards, quotations from vendors or information from the operating cost database and information from the process design criteria underline the basis of the estimate (refer JORC Table 1 attached for additional information).

Tailings

Tailings will be thickened and pumped to a conventional paddock/cross valley fill type TSF. The TSF will require storage of approximately 5.64Mt of non-acid-forming tailings produced at a rate of up to 0.45Mtpa for a design life of 14 years.

Based upon a proposed location within a natural saddle feature, an initial TSF options assessment for an aboveground TSF was undertaken. From this assessment, a centreline-raised, single-cell TSF located north of the process plant was selected for development. The centreline construction method minimises the reliance on the deposited tailings for strength and stability of the perimeter embankment, whilst utilising the mine waste material for construction of the raises.

The starter embankment will then be progressively raised.

The starter embankment will be constructed of compacted low permeability fill material sourced from the pit pre-strip operations and impoundment excavation works. Subsequent raises will be constructed of low permeability fill on the upstream section of the embankment, with mine waste material being utilised in the downstream zone of the embankment.

The tailings will be pumped to the TSF as a slurry at a target solids concentration of 45% solids by mass. Deposition into the TSF will take place through spigots located along the perimeter embankments. A floating pontoon is proposed throughout the life of facility as it is anticipated that there will not be a centrally located pond for many years into the life of the facility. The water will be sent to a return water pond in the processing plant area for reuse.

The results of a stability analysis indicate that the estimated factor of safety against failure is greater than the Australian National Committee on Large Dams (ANCOLD) (2012) recommended minimum values. The TSF is classified as a Category 1 dam according to DMIRS (2013) (refer to the JORC Code (2012) Table 1 which is attached for additional information).

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Roads – Page 23 (Page 17 of presentation)

Project access is proposed via the South Coast Highway. The new site access roads will be constructed in accordance with appropriate Restricted Access Vehicle ("RAV") requirements (refer to the JORC Code (2012) Table 1 which is attached for additional information).

Marketing – Page 25 (Page 19 of presentation)

Revenue estimates are based on independent market pricing and life of mine concentrate production of 745,022t at an average 52,000tpa of production.

The basket price used in the model has been calculated based on pricing obtained from Roskill Information Services Ltd's latest market report: "Natural and Synthetic Graphite: Outlook to 2028, 12th Edition" ("Roskill Report") (refer to the JORC Code (2012) Table 1 which is attached for additional information).

Pricing – Page 26 (Page 20 of presentation)

Graphite, a form of carbon, has two main types - natural and synthetic. The combined natural and synthetic graphite has a market size of some 2.52 million tonnes (2018). Natural graphite accounts for 38% of this market. The graphite market is an opaque market where most information is not readily available and market analysis is based on limited available data combined with estimations.

The refractory market still has the biggest share of graphite consumption and graphite is mainly used in magnesia carbon bricks for iron and steel production. Battery markets, especially lithium-ion batteries, represent the fastest growing markets and their main demand driver is electric vehicles. Prices are expected to rise in the long-term with rapid growth in demand from the lithium-ion battery industry underpinned by uptake of electric vehicles and energy storage systems.

Roskill forecasts that demand for natural graphite will grow from 947kt in 2018 to 1,686kt in 2028 – a Capital Annual Growth Rate ("CAGR") of some 5.9% pa. Demand from battery markets will grow by 483% from 2018 to 2028 or at a CAGR of 19% (refer to the JORC Code (2012) Table 1 which is attached for additional information).

Risk Management

75% of the risks are in the Medium and Management Action categories, with the balance of the total risks in the Low range. This is typical of mining projects that have not yet received

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environmental approvals to allow construction to commence. The Project is likely to result in a lower risk profile once additional controls are effectively applied.

It is the intention of the Company to implement a vertically integrated development strategy that will provide a broader range of higher value products and diversify the risks associated with supplying the traditional graphite market.

MUNGLINUP GRAPHITE PROJECT RISK MATRIX

		Consequences				
		Low (1)	Minor (2)	Moderate (3)	Major (4)	Critical (5)
Likelihood	Almost Certain (A)					
	Likely (B)		• Construction Risk	• Ramp up		
	Moderate (C)		• Geotechnical Stability • Acidic and Waste Rock Filter washing performance • Environmental Management - Operations & Construction • Stir Mill Performance	• Development Schedule - Corporate • Provision of Vendor Test Samples • Product Handling • Disenfranchised TO • Dispersive and erodible waste material • Water • General Site Safety • Environment and Permitting Approvals	• Legal • Operating Cost • Graphite Price	
	Unlikely (D)		• Exchange Rate Fluctuations and Escalation • Pit Inflow • Availability of Contractors • Extreme Weather Impacts • Product Logistics • NGO's • Consumables (Diesel/LNG) Supply	• Crusher and scrubber performance • Insurances • Resource Risk • Flotation Performance Risk • Legal • Community • Owners Costs • Product Quality • Medical Systems and Facilities • Ore Representativeness and Variability	• Legal • Environment • Production Capacity • Tailings Storage Facility (TSF) • Tailings Storage Facility (TSF)	• Tailings Storage Facility (TSF)
	Rare (E)		• Site Layout • Capital Cost	• Plant Performance • Port Export	• Onsite Traffic Movements • Road Safety Risk	• Environment and Permitting Approvals

Legend	Low	Medium	Management Action	Priority Action

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END

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About Mineral Commodities Ltd:

Mineral Commodities Ltd (ASX: MRC) is a global mining and development company with a primary focus on the development of high-grade mineral deposits within the industrial and battery minerals sectors.

The Company is a leading producer of zircon, rutile, garnet and ilmenite concentrates through its Tormin Mineral Sands Operation, located on the Western Cape of South Africa. In October 2019, the Company completed the acquisition of Skaland Graphite AS, the owner of the world's highest-grade operating flake graphite mine and one of the only producers in Europe. The planned development of the Munglinup Graphite Project, located in Western Australia, builds on the Skaland acquisition and is a further step toward an integrated, downstream value-adding strategy which aims to capitalise on the fast-growing demand for sustainably manufactured lithium-ion batteries.

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JORC Code, 2012 Edition – Table 1
Munglinup Graphite Deposit

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections)

Criteria	Commentary
Sampling techniques	• The current resource database consists of 161 air core holes, 26 RC holes and 46 diamond holes representing 8,332m of drilling and 3,569 analysed drill samples. • Air core (undertaken by Graphite Australia) ore zone intervals were sampled every metre using a scoop spear and the material bagged and numbered. Waste was not sampled except for a small buffer either side of the mineralisation. • Diamond drilling (undertaken by Graphite Australia) ore zone intervals were sampled every metre except for ore boundaries where a longer or shorter interval was taken. Waste was not sampled except for a small buffer either side of the mineralisation.
Drilling techniques	• Diamond drilling was done using HQ triple tube. • The mineralisation occurs from surface and drilling was done to a maximum of 91m depth.
Drill sample recovery	• No continuous data was recorded on core or chip recovery. Only poor sample quality and recovery were recorded for air core. • Due to the style of the deposit it is considered that any material loss is not significant to the estimation of mineralisation. However, statistical analysis of core recovery is still to be completed.
Logging	• Holes were initially logged by on-site geologists. Diamond core was relogged and resampled in 2016. • The data and results obtained from the 2012-2013 (Graphite Australia) drilling campaign were compared with the new logging and lab results from 2016 (AEMCO) as well as the historical logging and grades from the 1986 diamond holes by Sons of Gwalia. The two datasets were correlated to an acceptable level. • A comprehensive logging system was developed and included alteration (type, style and intensity), grain size, rock type/lithology, colour, minerals, textures, fabric, parent rock (where fresh), sedimentary setting and, graphite class and grade. • Geotechnical aspects in the form of RQD parameters were also recorded for the diamond core as well as specific structures and details in this regard, eg alpha angles.
Sub-sampling techniques and sample preparation	• Air core was sampled using a scoop spear. • Diamond core was cut by a diamond impregnated blade core saw and half core sampled. Resampling of the remaining core in 2016 for data validation purposes (422 core samples including 26 duplicates and 19 repeat samples) used quarter core. • Duplicates (quarter core) were taken every 20 metres during the Graphite Australia drilling program.
Quality of assay data and laboratory tests	• Standards were inserted every 20 metres. No blanks were used in addition to normal laboratory QA/QC protocols. • Sample analysis was undertaken by Nagrom in Perth for the Graphite Australia samples. • The graphite content is reported as Total Graphitic Carbon (TGC). Prepared samples are dissolved in HCl over heat until all carbonate material is removed.

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Criteria	Commentary
	The residue is then heated to drive off organic content. The final residue is combusted in oxygen with a Carbon-Sulphur Analyser and analysed for TGC. • Sample analysis was undertaken by Analabs in Perth for the Gwalia Minerals NL samples. Two methods were used: • Fixed carbon (>40%C) – C graphite is determined as an expression of fixed carbon, which is calculated by subtracting the sum of the percentages of moisture in the sample, volatile matter and ash from 100 (BS1016 methodology). • Fixed carbon (<40%C) - the sample is washed with organic solvents, filtered and washed with NaOH solution. The sample is then attacked with hot 1:1 HCL to remove carbonates, washed and dried at 105°C, the residue is analysed for carbon by converting the carbon to CO2 in a Leco furnace and measuring by infra-red. • Eleven check samples (pulps) from Analabs were sent to Classic Laboratories for cross checks. Classic Laboratories washed the samples with dilute HCL to remove carbonates, ash at 450°C to remove organic carbon and assay by Leco furnace for the remaining fixed carbon/C graphite. Check assays (>10% fixed carbon) were all within ±10% of the original Analabs assay. Analabs assays within the range 5% - 10% fixed carbon was approximately 15% lower than Classic's check assays.
Verification of sampling and assaying	• Four twin holes were drilled by Graphite Australia near (8-14m) the historical diamond holes by Sons of Gwalia. • The database containing drilling data and results was provided by Graphite Australia. A review of the data was done by the project field geologist Mr Luke Forti and the accuracy of the data was discussed with him during a number of meetings with AEMCO during 2015. Confirmation of the integrity and accuracy of the data was provided. • A visual review of the diamond core was then done by AEMCO in 2016 to confirm the historical logging by Graphite Australia. Any outstanding information was recovered from the diamond core and updated geological logs were created. • Diamond core was relogged and resampled in 2016. 422 core samples were re-analysed by Nagrom during April 2016, including 26 duplicate and 19 repeat samples to confirm grade results. GGC01, GGC08 & GGC09 standards were used. • The data and results obtained from the 2012-2013 (Graphite Australia) drilling campaign were compared with the new logging and lab results from 2016 (AEMCO) as well as the historical logging and grades from the 1986 diamond holes by Sons of Gwalia. Any discrepancies or errors were either corrected or the results rejected.
Location of data points	• All exploration drill hole collars were resurveyed to 0.05m accuracy by Esperance Surveys in July 2016. In total 90% (179 holes) were re-surveyed to confirm location integrity. Average variation from the original field survey in all directions was less than 2m. • Holes drilled since 2016 have had their collars picked up by GPS. These hole collars will be surveyed in the future. • Air core holes were down hole surveyed at the end of the hole only. Diamond drill holes were surveyed at 30m depth and the end of hole. • Local grids were established at each of the prospects then later converted to GDA94. Hole collars were originally surveyed by GPS only.
Data spacing and distribution	• Drill spacing: ○ Halberts Main Zone: (Drill Grid 40 x 20m to 50 x 20m).

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Criteria	Commentary
	○ Halberts South Zone: (Drill Grid 40 x 20 & 40 x 10 infill) ○ Harris Area: (Drill Grid 40 x 20m) ○ Wright West Area: (Drill Grid 40 x 20) ○ Wright East (McCarthy) Area: (Drill Grid 40 x 10)
Orientation of data in relation to geological structure	• The deposits were drilled at approximately -60° to intersect the mineralised zones approximately orthogonal to the interpreted dip and strike of the geological units.
Sample security	• Graphite Australia followed a disciplined QA/QC process as is evident from their database and chain of command documents. AEMCO followed the same procedure and personally took all resampled material to Nagrom and recovered the processed sample material for storage with the remaining core and air core samples at a secured location in Welshpool, WA.
Audits or reviews	• An audit was conducted by Coffey Mining Pty Ltd in 2011 prior to the additional drilling undertaken by Graphite Australia. The review stated: "Resources and reserves are assessed to be non-JORC compliant, given the age and the lack of available core. However, given the level of documentation provided, and the extent to which an auditable trail exists in relation to the modelled resources and reserves, the metrics presented are credible and serve as the basis for project decision-making." • The 2012-2013 exploration work done by Graphite Australia was reviewed and completed by AEMCO in 2015 and 2016 and from this review a maiden JORC 2012 resource was determined.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section)

Criteria	Commentary
Mineral tenement and land tenure status	• The tenements (M74/75 & E74/505) are situated on the Ravensthorpe SI 51-5 and North-Over 3031, 1:250,000 and 1:100,000 geological sheets respectively. • Mining Lease 74/245 was granted on 26 August 2010 for a term of 21 years. The Lease is 685 hectares in area. • Exploration Licence 74/505 of two-block size was granted on 23 October 2012 for a period of 5 years. • Gold Terrace Pty Ltd is the current registered owner of the Munglinup Mining Lease (M74/245) and Exploration Licence E74/505. • There is a caveat on the tenements relating to a 2% gross royalty liability with Adelaide Prospecting as the beneficiary. • The fully granted mining lease is valid to August 2031. • The tenements are located in a fully gazetted mining reserve, with no native title or private land ownership issues.
Exploration done by other parties	• Metals Exploration NL – (1971-1972) • Norseman Gold Mines – (1979-1980) • Pioneer Concrete – (1985-1986) • Gwalia Minerals NL – (1988 – 1989) • Sons of Gwalia – Gwalia Minerals: Feasibility Studies – (1989 to 1991) • Adelaide Prospecting – (2007-2010)

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Criteria	Commentary
	• Graphite Australia (2010-2013) • Gold Terrace (2014–2016)
Geology	• The Munglinup area comprises Archean to Paleoproterozoic, metamorphosed granitic and other metamorphic rocks of the Albany–Fraser Orogen, typically hornblende (± garnet) gneiss and migmatite. • Within the gneissic rock mass, rocks containing the Munglinup graphite deposits consist of a succession of tightly folded metasedimentary rocks with a consistent dip from north north east to the south. • The classification scheme most widely accepted for graphite deposits was introduced by Cameron (1960). It classifies known graphite deposits into five categories reflecting the different types of graphite. • Using this classification scheme, it is most likely that the Munglinup deposit can be characterised as a type 1, disseminated flake graphite in silica-rich meta-sediments deposit.
Drill hole Information	• No exploration results are being reported.
Data aggregation methods	• No exploration results are being reported.
Relationship between mineralisation widths and intercept lengths	• Inclined air core and diamond drilling (HQ3) was done to try and intersect the different graphite zones as close to true width as possible. Average dip angle was 60°.
Diagrams	• No exploration results are being reported.
Balanced reporting	• No exploration results are being reported.
Other substantive exploration data	• No exploration results are being reported.
Further work	• To be announced to the market in the near future.

Section 3 Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section)

Criteria	Commentary
Database integrity	• Data is currently stored in a secure third party (Maxwell Geoscience) cloud hosted and maintained geological database solution (WebShed). A review of the data was done by the project field geologist Mr. Luke Forti and the accuracy of the data was discussed with him during a number of meetings with AEMCO during 2015. Confirmation of the integrity and accuracy of the data was provided. • A visual review of the diamond core was then done by AEMCO in 2016 to confirm the historical logging by Graphite Australia. Any outstanding information was recovered from the diamond core and updated geological logs were created.

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Criteria	Commentary
	• Diamond core was relogged and resampled in 2016. 422 core samples were re-analysed by Nagrom during April 2016, including 26 duplicate and 19 repeat samples to confirm grade results. GGC01, GGC08 & GGC09 standards were used. • The data and results obtained from the 2012-2013 (Graphite Australia) drilling campaign were compared with the new logging and lab results from 2016 (AEMCO) as well as the historical logging and grades from the 1986 diamond holes by Sons of Gwalia. Any discrepancies or errors were either corrected or the results rejected.
Site visits	• No site visit was undertaken as all drilling, survey work and site rehabilitation had been completed before this resource assessment started.
Geological interpretation	• The overall continuity of the graphitic schist is very strong yet local geometric complexity can be high. • Geological logging, and to a minor degree assay, have been used to generate estimation domains. Unassayed intervals have been set to zero before estimation. The minimum interpreted thickness of mineralisation and internal waste was 1m. • The strike and dip of the deposit is well understood. The mineralisation is sometimes tabular but can also be geometrically complex. Mineralisation pinches and swells and bifurcates. There may also be small scale faulting and faulting which is still not well understood and, while probably not impacting on global tonnes and grade, can impact significantly on the local geometry.
Dimensions	• The mineralised zones consist of numerous thin (2-20m wide) steeply dipping folded zones reflecting a cover nappe system with late stage granite and pegmatite intrusions. • Halberts Main Zone: o Length: 730m o Width: 90-130m o Depth: surface to -90m • Halberts South Zone: o Length: 560m o Width: 20-50m o Depth: surface to -60m • Harris Area: o Length: 435m o Width: 30-70m o Depth: surface to -35m • McCarthy West Area: o Length: 290m o Width: 100-110m o Depth: surface to -55m • McCarthy East Area: o Length: 260m o Width: 12-20m o Depth: surface to -30m
Estimation and modelling techniques	• Leapfrog Geo was used to model the lithology-based estimation domains. • Exploratory data analysis and variography was completed in Isatis while estimation occurred in Minesight. • 1m composites were used for estimation. The total graphitic carbon has a low coefficient of variation of about one and top cuts were required.

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Criteria	Commentary
	• Kriging was into 5m x 5m x 5m blocks while the drill hole spacing was generally 40x10m to 40x20m. Small blocks were required because the modelled mineralisation can be as narrow as 1m. • Sample to block distances are generally with 20-30m for Indicated, while Inferred resources are generally within 50m. • Domain boundaries were treated as hard during estimation. • Anisotropic search distances were used. • Minimum of six composites to estimate a block except for the Halberts Main area where the minimum was reduced to 3 so that all blocks could be estimated. • No quadrant or octant searching was used. • Maximum number of 30 composites to estimate a block except for the McCarthy area where this reduced to a maximum of 15. • Discretisation of 5x5x5. • Search dimensions of 300m x 300m x 50m. • The kriged estimate was validated by alternative nearest neighbour, inverse distance and kriged estimates. • Estimate was visually checked against composite grades and swath plots were generated. • No byproducts are present. • No deleterious elements have been estimated.
Moisture	• The resource tonnages are based on a dry basis at a Bulk Density of 1.
Cut-off parameters	• The current reported resource was declared at a cut-off grade of 5%. The industry standard median grade for commercial graphite mine development is considered to be approximately 7-10% TGC. The cashflow model developed for mine optimisation included some blocks as low as circa 6% TGC as economic, given favourable metallurgical response estimations and material location (ie short haul distances).
Mining factors or assumptions	• Mining of the deposit will be by open pit surface mining methods involving standard truck and haul mining techniques. • It has been assumed that no drill and blast will be required given the weathered nature of the deposit and corresponding weak material strength.
Metallurgical factors or assumptions	• Extensive metallurgical testing has been done on the deposit which include the following studies: • Amdel (for Picon) – 1986 • Leach and Flotation test work – Chemistry Centre – 1990 • Settling Tests – Chemistry Centre – 1991 • Flotation Tests – Chemistry Centre – 1991 • Screening Test – Chemistry Centre - 1992 • Coffey Mining - 2011 • Metallurgical study – TF Brittliffe – 2011 • Nagrom tests 2011-2016 and Petrographical studies by Roger Townend and Associates • BatteryLimits supervised testwork at ALS Metallurgy labs in Perth – 2018 ○ See Section 4 for more detail
Bulk density	• The bulk density is based on historical density calculation for the material at • 2.0 g/cm3 • The host geology comprises weathered metamorphic material. Visual inspection of core indicates little loss of material due to vugs or discontinuities.

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Criteria	Commentary
	• All material within the mineralisation domains were assumed to be a combination of graphitic gneiss, graphitic ironstone and graphitic magnesite.
Classification	• Classification is Indicated for 40m spaced drilling. • Inferred resources are up to 100m from the nearest drill hole but extrapolation distances of 30-50m would be more common. Inferred resources are generally in areas where the mineralisation is considered thicker and more continuous. • These resource classifications are considered appropriate by the competent person for the style of mineralisation and quality of data.
Audits or reviews	• No formal review or audit of the Mineral Resource model has been completed. • The model was informally reviewed by Mr. Andrew Scogings of CSA Global who is a highly experienced geologist with expert knowledge of industrial minerals exploration, mining and processing, product development, market applications and commercialisation processes. Andrew has published several papers on the requirements of JORC 2012 Clause 49 and is an AIG Registered Professional Geologist specialising in industrial minerals.
Discussion of relative accuracy/ confidence	• The Munglinup graphite deposit has been mapped, drilled, mined and investigated numerous times over the past 100 years. The high-grade nature of the resource and its potential is well documented. • While large scale continuity of the mineralised domain is good, variogram ranges are short and local estimation accuracy is often low. • The resource estimate compares favourably with historical production grades of 19%. • Conditional simulations of total graphitic carbon were generated in 2019 for Halberts Main. The indicated resource was divided into three elevation-based zones each equating to about 12 months production. The uncertainty in predicted tonnes of graphite was ± 14%. This, however, does not include uncertainty for the geological interpretation and density which may be significant.

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• The Mineral Resource was updated in April 2019. Mr. Chris De-Vitry is the Mineral Resources Competent Person for the purposes of the Mineral Resource Estimate as defined and in accordance with the JORC Code 2012. • Leapfrog Geo was used to model the lithology-based estimation domains. • Exploratory data analysis and variography were completed in Isatis while estimation occurred in Minesight. • 1m composites were used for estimation. The total graphitic carbon has a low coefficient of variation of about one and top cuts were required. • Kriging was into 5m x 5m x 5m blocks while the drill hole spacing was generally 40x10m to 40x20m. Small blocks were required because the modelled mineralisation can be as narrow as 1m. • Sample to block distances are generally with 20-30m for Indicated, while Inferred resources are generally within 50m. • Domain boundaries were treated as hard during estimation.

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Criteria	Commentary
	• Anisotropic search distances were used. • Minimum of six composites to estimate a block except for the Halberts Main area where the minimum was reduced to 3 so that all blocks could be estimated. • No quadrant or octant searching were used. • Maximum number of 30 composites to estimate a block except for the McCarthy area where this reduced to a maximum of 15. • Discretisation of 5x5x5. • Search dimensions of 300m x 300m x 50m. • The kriged estimate was validated by alternative nearest neighbour, inverse distance and kriged estimates. • Estimate was visually checked against composite grades and swath plots were generated. • No byproducts are present. • No deleterious elements have been estimated.
Site visits	• Numerous site visits have been undertaken since October 2017. The nearby towns of Ravensthorpe and Esperance have also been visited to assess regional infrastructure and support capabilities. Historical core from the site has also been examined at various times by both the Mineral Resource and Ore Reserve CPs. • Surface mineralisation was examined along with locating of previous drill collars and review of recent drilling programs while being conducted. Access and exploration of possible mining issues were assessed along with a general geographic overview of the area.
Study status	• This study is assessed as being at a Definitive Feasibility Study Level. • Historical study work on the Munglinup Deposit is extensive. • The Definitive Feasibility Study evaluated geology and resource, mining, metallurgy, process plant and tailings, infrastructure and logistics, environment and permitting, human resources, marketing, implementation plan and schedule, capital and operating costs, financial assessment, risk management and other activities/issues that could impact the proposed operation as contained in the DFS. • The DFS considered the technical, engineering and cost components, as well as health and safety, and social and community impacts • Metallurgical testwork shows that an acceptable minimum level of recovery and concentrate grade can be obtained with confidence.
Cut-off parameters	• A simplified cash flow script was developed to generate at a block level all of the required attributes to calculate the cashflow grades for the proposed processing permutation for subsequent use in pit optimisation and strategic mine schedule optimisation. • The basis for the application of the cut-off grade is a simplified variable cash flow per tonne. This approach provides the most mathematically efficient inputs to solve the objective function as used consistently in the optimisation models developed, which is to maximise the real, pre-tax NPV. • The cash flow script provides the linkage between the block model, the metallurgy models and the scheduling models and therefore needs to accurately reflect the input assumptions. The cash flow script, and the cash flow grade which it generates is current industry best practice, and supersedes other forms of cut-off grade such as a graphite break-even estimation as used in the historical studies.

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	• The cash flow script was built with the current economic assumptions to accurately reflect the proposed operating cost profiles. The throughput and recovery calculation steps were based on the ALS testwork throughput and recovery estimations. • Blocks where the cash flow per tonne is positive are designated ore and negative blocks designated waste.
Mining factors or assumptions	• The pit shells were developed in Whittle 4x using the variable cash flow cut-off grade estimated in the block model. The optimisation shells selected comprised 13 open pits, mined over 2 stages, which initially target the higher value areas earlier in the mining plan. The stage 1 pits are optimised on the Measured and Indicated material while stage 2 optimisations include Inferred material. • A revenue factor of 1 was used for the stage 1 shells and 0.45 was used for the stage 2 shells. The lower revenue factor used in the stage 2 shells was deemed appropriate given the lower geological confidence. This resulted in selection of inferred material that is likely well above the cut-off grade and robust in terms of remaining economic within the variability of other modifying factors. • Dilution was set to 5% and ore recovery at 3% • All the selected pit shells had detailed pit designs created which aligned with the shells while retaining the geotechnical recommendations provided by Mining One. • The deposits will be mined in multiple stages using conventional open pit operation and will utilise conventional load-haul mining methods. Each bench will be mined using 130 tonne to 150 tonne class excavators and 100 tonne class rigid frame trucks. • A minimum mining width for pits of 35 metres based on the use of CAT 777 class rigid frame trucks. • Haul road widths designed to 22m for dual lane traffic and 15m for single lane, based on the use of CAT 777 class rigid frame trucks, with all ramp gradients to be limited to 1:10 (10%). • Mineralisation extends to surface so only limited pioneering and soil collection works are required. There is no pre-strip. • The high-grade nature of the deposit results in pit optimisation shell sizes increasing incrementally with revenue factor. • Access to the area is straight forward with council maintained roads available to within 2 kilometres of the mining area. • The topography is gently undulating rises and it is anticipated that no significant issues associated with mining are likely. • Historical work included a systematic examination of drill core to assess the requirement for drill and blast during mining and to assess open pit stability. The examination was based largely on RQD parameters and concluded that drill/blast of the ore zone was unlikely to be necessary or desirable. Drill and blast of the west wall gneiss may however be required at depth. This has been costed in the contract mining proposals but not included in the financial model at this stage. Further detailed work on material hardness at depth will be conducted when appropriate. • Infrastructure requirements for the selected mining method are minimal. Annual material movement is planned to be limited to 3.5Mt per annum for the first 3 years of operation then reducing to a maximum of 3Mt per annum. • This level of mining activity is minor and will only require the most basic infrastructure such as a small workshop, office, crib and ablution block and

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	equipment hard stand.
	• The average strip ratio is 5:1 (waste:ore).
	• Ore requirements for the process plant are
	  o 400kt per annum for the first five years at an average feed grade of 15.7% TGC.
	  o 500kt per annum for the remaining mine life at an average feed grade of 11.1% TGC (representing a 41% reduction in feed grade which will be compensated for by a 25% increase in throughput).
	• Based on the block model, the total mined mine waste rock volumes are expected to be approximately 35.3 million tonnes over a 14 year mine life. This equates to 19.3 million cubic meters of loose material at an average in-situ bulk density of 2.45 and a swell factor post mining of 35%.
	• Halberts Main will be required for waste dumping once the pit has been finalised at the end of 2026. Available volume in Halberts Main is 6.3 million cubic metres. Total waste material remaining post completion of the Halberts Main pit is 9.79 million loose cubic metres.

Metallurgical factors or assumptions	• The metallurgical process proposed comprises standard graphite flotation processing. Flotation is a standard processing method for graphite flake deposits. • Flotation technology is well tested and understood. • Significant historical metallurgical testwork has been undertaken. Overall, more than 20 specific metallurgical studies were undertaken on the Munglinup Graphite mineralisation, predominantly in the late 1980s and early 1990s. In 2017, a metallurgical testwork program was undertaken at ALS Laboratory (ALS) in Perth to assess the ore's amenability to beneficiation by gravity and froth flotation. The results from this testwork program were used to support the process design and engineering for the 2017 PFS. In 2018 and 2019 further drilling was conducted to generate samples for additional metallurgical testwork programs to support the DFS. • An 8t bulk sample was extracted from the Halberts Main deposit to be used for metallurgical test work undertaken by Nagrom in 2011. This sample does include material from the three mineralisation types. The sample has ultimately been deemed only partially representative as it does not include material from depth. Future metallurgical testwork is utilising a master composite derived from historical drilling core and that has been selected to provide high representivity of the deposit. • The 2018 PFS testwork utilised core that had been drilled in 2013 in Halberts Main and Halberts South areas. The variability program utilised core from eight drill holes from the 2018 program, located at Halberts Main and Halberts South at varying depths and lithology.

Sample ID	TC (%)	TGC (%)	SiO2 (%)	S(t) (%)	Al (%)	Ca (%)	Fe (%)	Mg (%)
PFS Master Composite	19.2	16.9	33.0	0.06	4.28	1.20	13.6	3.68
Var1	11.9	7.20	17	0.04	4.96	1.00	19.0	9.36
Var2	36.2	31.5	36.4	0.04	5.72	1.30	2.00	1.32
Var3	27.6	24.9	42.4	0.04	7.28	1.00	3.68	0.84

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Var4	16.8	16.5	45.6	<0.02	5.72	<0.01	11.4	1.12
Var5	28.3	27.3	39.4	0.08	4.48	<0.01	10.5	0.40
Var6	17.4	16.8	41.2	0.06	5.00	0.20	15.5	0.64
Var7	13.6	14.0	45.4	0.1	4.96	0.30	14.7	0.76
Var8	23.4	22.1	43.4	0.04	8.92	<0.01	3.86	1.6
Var9	27.5	24.6	48.2	0.16	7.04	0.40	2.18	0.84
Var10	22.7	21.9	44.8	0.02	6.76	0.30	3.82	0.28
Var11	28.9	26.3	40.6	0.04	6.96	0.30	6.96	0.40
Var12	10.3	9.51	10.4	0.06	0.76	1.50	42.1	2.88
Var13	8.67	6.81	12.6	0.04	2.20	1.10	41.4	2.08
Var14	33.2	33.0	39.6	0.04	6.44	1.60	2.40	1.24
Var15	16.9	16.7	49.8	0.62	8.72	0.30	2.66	0.2
Var16	15.9	14.6	44.2	0.02	7.32	0.20	0.48	3.68
Var17	18.2	16.8	22.4	0.02	9.68	0.10	10.0	3.36
Var18	9.36	8.79	14.2	0.04	4.4	0.40	33.2	0.48
Var19	24.8	24.3	27.2	0.04	9.04	<0.01	9.76	0.12
Var20	13.2	12.8	41.8	2.34	6.32	0.20	6.50	0.64
DFS Master Composite	16.3	14.3	33.0	0.23	6.64	2.00	9.86	2.96

- Comminution testwork was undertaken on the Master Composite, near surface scrubber feed samples that were relatively soft, and additional samples targeted to provide more spatial variability as well as more competent material based on visual selection of the core. The tests included:
  - SAG Mill Comminution test (SMC)
  - Bond Ball Work Index (BBWi)
  - Bond Rod Work Index (BRWi)
  - Bond Abrasion Index (Ai)
- The ore is naturally very friable, weathered and can generally be considered to be soft.
- Initial flotation testwork was undertaken on the variability composites of Halberts Main and Halberts South at varying depths and lithology. The TGC recoveries were variable ranging from 56.0 to 97.5 % within the distribution. The composites with poor recoveries were either those in the ironstone-rich or near surface zones. A size analysis of the final concentrates showed that all these composites contained little amounts of coarse flakes with most of the material in the -75 µm size fraction.
- The feed size P100 of 1000 µm was selected as the primary grind for the rougher circuit. Generally, the test procedure involved desliming the ground material at 25µm followed by rougher flotation. The rougher concentrate then underwent a secondary grind, as there were some coarse composites that needed to be liberated, before undergoing multiple cleaning stages. Prior to each cleaning stage the concentrate was reground in a stirred mill using ceramic media. This procedure aimed to increase graphite particle liberation whilst trying to avoid

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the break-up of coarser flakes.

- The flotation reagent scheme was relatively simple, consisting of kerosene as the collector, and a frother. All flotation tests were carried out at natural pH.
- The TGC recoveries were variable ranging from 56.0% to 97.5%. The results showed that the high-grade final concentrates can be consistently produced with TGC grades ranging from 95.0% to 98.3% after 5 stages of cleaner flotation.
- The results showed that the coarse flake fraction (+150µm) can be maintained at around 50% proportion of the concentrate at high average TGC grades (up to 97.7%) and that high-grade fines (-150µm) concentrate can be produced with up to an average of 98.3% TGC.

Test ID	Final Concentrate				
	+150 µm (Coarse)		-150 µm (Fine)		Total TGC Recovery
	% Mass	% TGC Grade	% Mass	% TGC Grade	
BF1273	44.0	97.3	56.0	93.9	88.7
BF1281	48.4	97.7	51.6	94.2	86.6
BF1282	56.2	95.2	43.8	91.0	89.4
BF1289	57.0	95.7	43.0	97.2	86.4
BF1304	47.7	96.5	52.3	94.1	87.1
BF1305	46.4	96.5	53.6	98.3	84.9
BF1306	54.1	97.4	45.9	97.9	84.6
BF1334	51.4	95.1	48.6	97.6	85.8
BF1360					83.9
BF1363	49.3	97.1	50.7	95.6	67.0
BF1371	57.9	89.7	42.1	97.1	86.3

- In 2019, further drilling was conducted to generate samples for a metallurgical testwork program to support the DFS.
- A DFS Master Composite was produced and test work focused on optimising the flake size distribution and final grades of the concentrate. The testwork also investigated adjusting reagent addition rates, the number of cleaning and recleaning flotation stages, the number of polishing grinds, alternate reagents and intermediate screening. Processing was generally in Perth water with additional tests conducted using site water.
- The results showed that the coarse flake fraction (+150µm) can be maintained at around 50% proportion of the concentrate at high average TGC grades (up to 97.7%) and that high-grade fines (-150µm) concentrate can be produced with up to an average of 98.3% TGC.
- A 480kg bulk sample of the DFS Master Composite was prepared and underwent large batch flotation tests in order to produce concentrate for vendor and marketing purposes. The flotation scheme and was based on the optimisation test work and utilised larger laboratory equipment. The coarse flake fraction was contained 48.6% of the mass with a TGC grade averaging 95.8%. The fines accounted for 51.4% of the mass with a TGC grade averaging 96.0%.

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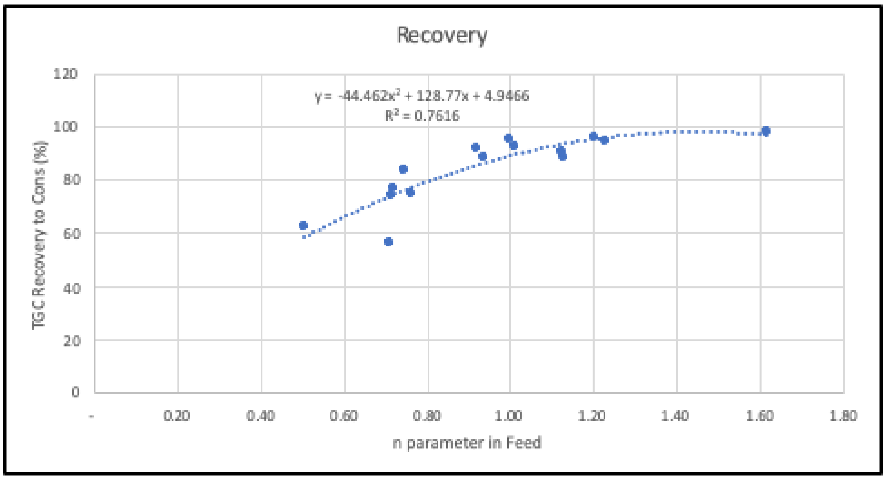
Flake Size	Micron (µm)	Mesh	Bulk sample Test BF1287	
			Mass (%)	Assay TGC (%)
Jumbo	300 – 500	50	17.7	96.0
Large	180 – 300	+80 -50	24.5	95.5
Medium	150 – 180	+100 -80	6.43	96.1
Small	75 – 150	+200-100	24.6	97.8
Fines	– 75	-200	26.8	94.4
Calculated P_{80} (µm) and TGC Grade (%)			**289**	**95.8**

- Testwork also included scrubbing, thickening, filtration, and rheology.
- Thickener testwork results indicated that both tailings and concentrate can be thickened by high rate thickening over a range of fluxes. The tailings reached densities up to 50.2% solids (w/w) while the final concentrate reached densities up to 36.8% solids (w/w).
- Comparative filtration testwork found that the most efficient method was pressure filtration over vacuum filtration. A final cake moisture of around 15% w/w was achieved with extensive air blowing.
- Graphite flake size distribution is set using a Rosin-Rammler Regression model.
- Analysis of the variability test work data shows that the n (dispersion) parameter on the Rosin-Rammler TGC feed distribution is a good predictor of the TGC recovery.



- The distribution was also used to determine the product flake size distribution. This estimation also correlated well with the variability testwork data.

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	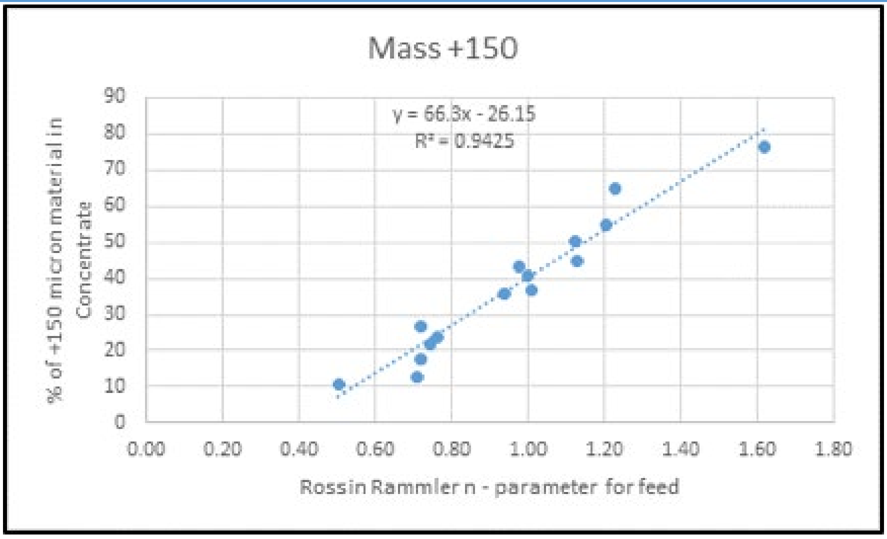 • No specific allowances have been made for deleterious elements. Any non-graphite material that reports to the graphite concentrate is deemed to be dilutionary in nature only and does not attract any specific penalties beyond the reduction in concentrate price based on the graphite concentrate purity as is standard in the industry. • Both historical and recent work has been done on the mineralogy of the deposit. The latest petrographical study was conducted on 12 samples from drill cores that are representative of the deposit. The petrographical nature of the graphite mineralisation at Munglinup is well understood and shows that the final product will be able to meet the required specifications mineralogically.
Environmental	• Significant environmental assessment work has been undertaken. The deposit lies entirely within a granted mining lease and information from the DMR suggests that only limited additional information will be required to proceed with operations. • The potential mine waste associated with the Project is dominated by Non-Acid Forming (NAF) and uncertain material, a small proportion of the waste is Potentially Acid Forming (PAF). The PAF material will need to be managed during operations. The Project wastes were also found to contain metals above local soil concentration that can be potentially harmful to the environment such as arsenic, copper, lead, nickel and zinc, however only copper, nickel and lead are of concern and may require specific management during operation and closure. No metals were found to exceed health investigation level. All materials tested were found to have Exchangeable Sodium Percent (ESP) values >15% indicating that the wastes are strongly sodic and potentially dispersive. • Flood assessments for a 1-in-100 and 1-in-2000 year flood events are not envisaged to impact on the Project, with the exception of a small creek line adjacent to the Halberts Main pit. • Results of geochemical characterisation associated with two tailings solids and one tailings liquor. The results indicate that the Munglinup tailings are Potentially Acid Neutralising (PAN), and that molybdenum and selenium are potential constituents of concern in leachate from dry tailings. • Seven soil types have been identified and mapped within the Project area. The majority of soil types within the Project are nutrient deficient, and typically very shallow (2-5cm) with an organic material layer which included leaf litter and

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	degrading material with topsoil. Four of the soil types show high ESP, and have a higher clay content and high sodium levels, which indicates that these soils are potentially dispersive (ISPL 2018). The most common soil type within the Project area is the Brown Loam Duplex, with the majority of available growth medium likely to come from this soil type (ISPL 2018). • The Project lies within the Esperance Coast Topographic Drainage Division and the Munglinup River sub-catchment, with drainage trending southwards via two main features, the Munglinup River and its tributary, Clayhole Creek. • A Munglinup River Assessment Report was completed by Wetland Research and Management in 2018. Concentrations of heavy metals are mostly below the limit of detection and are not of ecological concern. • Two vegetation surveys have been completed over the proposed Project area, one by Ecologia Environment in 2014 and the second by Woodman Environmental in 2018. • In 2018, a Phytophthora Dieback assessment was completed within the main Mining Area. This assessment found no Phytophthora Dieback infestations, however the majority of the vegetation within the Project was mapped as uninterpretable due to an insufficient coverage of reliable indicator species (Glevan Consulting 2018). • No known groundwater users are expected to be impacted by the Project groundwater abstraction. • Three fauna surveys have been completed across the Project Area, one in 2014 by Ecologia Environment and two by Red Dog Environmental in 2018. Field records from fauna surveys and database records determined the 85 fauna taxa were recorded from direct sightings and indirect evidence (scats, tracks and calls). Two conservation significant species have been recorded in the area, one an endangered species - Carnaby's Black Cockatoo and the second a priority 4 species – Quenda.

Infrastructure	• The mining lease is currently devoid of any structures or buildings. Access to the site from Munglinup township, 4km to the south, is by gravel road either from the west across the Munglinup River or by station tracks from the east. Both access roads are in need of an upgrade.
	• The Primary Process Plant has been designed comprising:
	  o a conventional comminution circuit with a sizer followed by scrubber and ball mill;
	  o flotation circuit with rougher, scavenger and cleaner sub-circuits, including attritioning mills between cleaner cells;
	  o product drying, classification and bagging back end; and
	  o tailings thickening and storage circuit
	• The process plant has a nameplate throughput of 400kt per annum however the comminution circuit has significant excess capacity given the smallest, off the shelf equipment available from manufacturers is oversized for Munglinup requirements. Additionally, the thickening tanks have been oversized to allow for a 25% increase to throughput should the feed grade drop by 25% or more. The drying, classification and bagged end of the circuit will not be impacted as the product tonnages will remain within the operational limits due to the reduced feed grade. It has been estimated that the capital requirement for increasing the throughput of the circuit to compensate for a similar reduction in feed grade is minimal and is included in the sustaining capital estimate.
	• The power requirements for the main process plant have been calculated at a

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	total connected load of 5.3 MW including all duty and standby equipment with an estimated average demand of the project being 2.5MW with a peak of 2.8MW. This running load was determined from the estimated plant load plus allowances for losses.
	• Power is proposed to be supplied by Powerwest with a 4.0 MW power station comprising 4 x containerised Jenbacher J320 - 1,057kWe reciprocating generator sets (gensets) operating with an n+1 strategy. The power station will supply power to the plant at 415V.
	• The power station will be fuelled by liquefied natural gas (LNG) supplied by EVOL LNG (a division of Wesfarmers), based on an onsite storage and vaporisation facility comprising a single 135 tonne LNG storage tank, associated ancillary equipment and telemetry systems with a storage capacity design allowance of a nominal 10-11 days.
	• The Project will transport product via road train combinations travelling 610 km from the Project via a third-party logistics provider (3PL) for storage, handling, packing of containers for export, and delivery to the Port of Fremantle (POF). Product will be loaded into bulka-bags with a nominal weight of one tonne prior to transport via tautliner trailers. Approximate product weight per trip is 60-65 metric tonnes.
	• The Esperance-Goldfields region has a deep pool of mining trained employees engaged primarily in the gold sector but also in other mining projects. It is planned that employees will be recruited to a base location in Esperance.
	• The Project is located approximated 105 km west of Esperance. Site access is proposed via the South Coast highway;
	  o North on Farmers Rd - 8.8 km
	  o West on Clayhole Rd - 3.6 km
	  o Primary site access eastern road – 6 km
	  o Secondary site access western road
	• The new site access roads will be constructed in accordance with appropriate Restricted Access Vehicle ("RAV") requirements. In addition, both Farmers and Clayhole Roads will be upgraded as required to comply with RAV road standards.
	• A borefield location has been investigated with several production bores drilled and pump tested to ensure that the borefield will support the operation. Water from the bores will be pumped to the raw water storage.
	• Generally, the project benefits from excellent infrastructure requiring only minimal additional expenditure.
	• Tailings will be thickened and pumped to a conventional paddock type TSF. The TSF will require storage of approximately 5.25 Mt of non-acid forming tailings produced at a rate of 0.35 Mtpa for a design life of 14 years.
	• The stability analysis of the Munglinup Graphite TSF embankment was carried out using the 2D limit equilibrium slope stability analysis software SlopeW (Geostudio 2018). Models were constructed for sections through both the south western corner and western embankments. Two representative cross-sections were analysed using the Morgenstern-Price method. The results of the stability analyses indicate that the estimated Factor of Safety against failure is greater than the Australian National Committee on Large Dams (ANCOLD) (2012) recommended minimum values.
	• A simplified dam break flow path assessment and hazard categorising was carried out for the TSF. The TSF is classified as a Category 1 dam according to DMIRS (2013). This classification is based on a High C hazard rating as defined

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Criteria	Commentary
	in ANCOLD (2012b) and an embankment height greater than 15m.
Costs	• Mondium has prepared a preliminary capital cost estimate for the Munglinup Graphite Project • The Project includes engineering, design, procurement and construction of a 400,000tpa graphite concentrator, using conventional crushing, scrubbing, screening, milling, flotation, drying, sizing and packaging technologies. • The capital estimate has been prepared by BatteryLimits, Mondium and MRC Graphite, with the capital cost estimate for the process plant, infrastructure, associated equipment and project management costs at+15/-5%.

Capital	Project Total US$M
Development Capital	55.5
Sustaining Capital	25.5
Pre-Strip Capital	4.3
Total	**85.3**

Capital	Project Total US$M
Construction Distributables	4.3
Treatment Plant Costs	21.5
Reagents & Plant Services	7.0
Infrastructure	8.5
Management Costs	8.0
Owners Project Costs	6.2
Total	**55.5**

- Contingency of US$5.7 million, representing some 11.5% of direct costs is included in the Project total development capex (US$55.5 million).
- Sustaining capital expenditure is US$25.5 million. This reflects the development capital of US$55.5 million being sustained at three percent per annum for the 14 years life of mine.
- Pre-development mining costs including mining mobilisation, clear and grub works, topsoil removal, haul road development and MRC Graphite costs are budgeted at US$4.3 million.
- The operating cost estimate for the Project includes all costs associated with mining, processing, infrastructure and site-based general and administration costs.
- The operating cost estimate has been prepared to an accuracy of ±15%.
- Industry standards, quotations from vendors or information from the operating cost database and information from the process design criteria underlie the basis of the estimate.
- The operating costs have been compiled by Mondium from a variety of sources and additional consultants including:
  - Budget quotations received from suppliers

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Criteria	Commentary
	o Operating cost database o Wages and salaries provided by MRC Graphite o General and Administration costs by MRC Graphite o HSEC costs inputs by ISPL and MRC Graphite o Product logistics by MRC Graphite o Estimates based on industry standards from similar operations o First principle estimates based on typical operating data • The mining operating cost estimates have been prepared by MRC Graphite, with inputs from Mining Contractor.

Operating Costs	US$ M	US$/t Sold
Mining	135.4	182
Processing	140.1	188
Product Logistics (CIF)	74.0	99
Royalties	46.7	63
Indirect Production Costs	30.8	41
Total (CIF)	**427.0**	**573**

Criteria	Commentary
	• Royalties have been calculated conservatively using a WA mineral royalty rate of five percent payable to the Western Australian government and a trailing residual royalty rate of an additional one percent payable to the original mining rights owners. Royalty payments are expected to be paid net of logistics expenditure. • All amounts have been modelled in US dollars with foreign estimated inflows/ outflows converted to US dollars at an average exchange rate forecast for the relevant transaction year. The forecast exchange rate used reflects long term exchange forecasts from a third-party foreign exchange provider and range from USD/AUD 0.68 to 0.70 over the life of mine.
Revenue factors	• Revenue from the project is derived from the sale of graphite product. Testwork has established that the Munglinup graphite product can be produced at a minimum of 94% graphite and, if produced to a minimum of 94% graphite in product, can expect to receive premium or near premium pricing levels. • Head grade delivered to the processing plant was derived from the underlying block model. A calculated recovery was used based on previous metallurgical testwork. • Testwork to date shows that there are no byproducts, coproducts or deleterious elements in the concentrate. • Revenue estimates are based on independent market pricing and life of mine concentrate production of 745,022t at an average 52,000tpa of production. • Prices are expected to rise in the long-term with rapid growth in demand from the lithium-ion battery industry underpinned by uptake of electric vehicles and energy storage systems. • The basket price used in the model has been calculated based on pricing

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Criteria	Commentary
	obtained from Roskill Information Services Ltd's latest market report: "Natural and Synthetic Graphite: Outlook to 2028, 12th Edition" ("Roskill Report"). • Forecast prices (real) for natural flake graphite (94-97% carbon) 2018-2028 for fine, medium and large flake were incorporated into the model. • Graphite prices were modelled from 2029 onwards in line with the 2028 forecast. • Prices for small flake product were modelled conservatively to largely reflect fine product pricing. • Prices for jumbo size flake graphite carry a 50-100% price premium over the published price of 94-97% carbon large size flake, with a 75% premium modelled. • Super jumbo products have been modelled with a further 40% premium on jumbo product. • Revenue estimates are base case only, reflecting average graphite grades of 95%. • MRC will continue test work to optimise grade performance towards 99% carbon concentrate production. Per the Roskill Report, prices of 99% carbon grade flake typically attract 55-65% higher prices than those of 95% carbon, representing significant upside to MRC.

Product	Price US$/t	Quantity (t)	Total US$'000
Super Jumbo	2,787	15,273	42,561
Jumbo	1,990	86,548	172,269
Large	1,130	155,053	175,228
Medium	1,077	62,851	67,712
Small	930	206,588	192,189
Fine	927	218,709	202,640
	1,144	**745,022**	**852,599**

Criteria	Commentary
Market assessment	• Graphite, a form of pure carbon, has two main types - natural and synthetic. The combined natural and aynthetic graphite has a market size of some 2.52 million tonnes (2018). Natural graphite accounts for 38% of this market. • The graphite market is an opaque market where most information is not readily available and market analysis is based on some available data combined with estimations. • Production of natural graphite, including all three forms of it (amorphous, flake, vein), is 0.95 million tpa. • China, with 60% share, is the biggest producer and seller. • The refractory market still has the biggest share in graphite consumption and graphite mainly goes into magnesia carbon bricks for iron and steel production. It is estimated that around 0.5 kg of natural graphite is consumed per tonne of steel, besides the given market share of 28%. In reality it is estimated that refractories consume 600,000 tonnes of graphite every year. • Total graphite market size could be beyond what was reported. It should be also considered that different graphite types could potentially substitute each other, and natural flake graphite is the only graphite type that could possibly substitute all other types of graphite, including synthetic graphite. • Battery markets, especially lithium-ion batteries, represent the fastest growing market and their main demand driver is electric vehicles.

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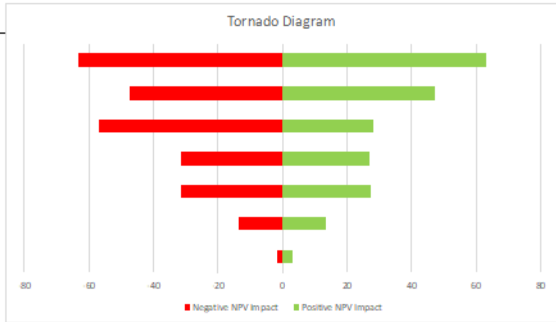
Criteria	Commentary

	• Both synthetic and natural graphite are mainly used as anode material in LiBs.
	• Natural graphite requires spheroidisation, purification and coating processes before being used in batteries.
	• To produce one tonne of natural spherical graphite, an average of two tonnes of natural graphite concentrate is required, mainly because of the rejection of non-spheroidised material during the process.
	• Natural spherical graphite and synthetic graphite are generally used together in the LiBs, with a mixture of 60% natural and 40% synthetic.
	• It is also estimated that 1 kg of graphite is required for each 1kWh of batteries.
	• Global production of LiBs was some 146 GWh in 2018. Roskill forecasts this level to grow to some 1,771 GWh in 2028. As a result, the demand for graphite is forecast to grow substantially.
	• Roskill forecasts that demand for natural graphite will grow from 947kt in 2018 to 1,686kt in 2028 – a CAGR of some 5.9% pa.
	• Prices for natural graphite with higher carbon content declined through the second half of 2018 and into 2019 with increasing supply, mainly from Africa, and a temporary slowdown in demand for lithium-ion batteries. Despite the decline they remain relatively high when compared to recent protracted lows.
	• Growing supply coupled with existing overcapacity in China is expected to push prices even lower through 2019. More supply will be available to come online through the early 2020s from the ramp-up/expansion of existing operations and potentially from some of the new projects currently under construction, although start-ups will likely be hindered by the current climate of weakening prices.
	• Such is the high level of forecast demand from lithium-ion batteries, however the prices could begin to strengthen again as early as 2021-22 with the market becoming tight in specific grades preferred for use in batteries.
	• Rising prices through the early 2020s could encourage a second wave of new projects, many of which are already well developed and might take it into production with the correct investment and offtake contracts in place. The release of new supply into the market could then result in a downwards recovery in prices towards 2028.
	• Based on MRC's market approach, the main focus will be:
	  o Possible value additions to our product, producing high purity graphite, developing expandable production etc.
	  o Specialty product markets, targeting alkaline batteries, lubricants, powder metallurgy, conductive additives, etc.
	  o Diversified and customer specific products, closely engaging with customers and developing the right products for the customers' requirements.
	  o Total value proposition: packaging, logistics, offering short delivery times, fast response times, consistent quality etc.
	• Short-Term (1 to 3 years) – Selling concentrates with the highest possible price and developing value-added products and markets. Expansion could be considered in the short-term.
	• Mid-Term (3 to 7 years) – Supplying the value-added product market (BAM).
	• Long-Term (>7 years) – New and downstream products (graphene for energy storage, coated spherical graphite etc).

Economic	• A discount rate of 7% (real). The discount rate applied reflects the weighted average cost of capital expected from debt funding the project. • Sensitivities of the NPV to changes in key assumptions have been analysed.

Criteria	Commentary
	These were run on the following key model assumptions: flake graphite pricing, flake graphite recovery, exchange rate, discount rate, operating costs, capital costs and construction schedule (capex timing). • In each case, the sensitivities run were regarded as a possible downside scenario and a possible upside scenario based on the historic experience of mining projects.

Assumption	Sensitivity	
Flake Graphite Pricing - Real	80% base	120% base
Opex	-20%	+20%
Flake Graphite Recovery	80% base	110% base
USD/AUD Exchange Rate	AUD 0.80	AUD 0.60
Discount rate	10%	5%
Capex Spend	-20%	+20%
Capex Timing	+6 mths	- 12 mths



Criteria	Commentary
	• The upside case for the flake graphite pricing forecast (120% base pricing forecast from Roskill) demonstrates a post-tax NPV at US$174M. The downside case (80% base pricing forecast from Roskill) demonstrates a post-tax NPV of US$48M. • All cash flows have been prepared in real terms, assuming 2019 dollars, with no inflation of graphite concentrate prices.
Social	• ML74/245 is a mining lease in the Esperance area granted on 26 August 2010 for a term of 21 years, expiring on 25 August 2031. • There are no plaints or other applications currently registered with respect to the tenement and no native title claims. • The tenement is in a Mining Reserve specifically set aside from agricultural release. The surrounding land use is primarily farmland. Proximal to mining lease 74/17A are reserves set aside for timber, recreation, water supply, parklands (recreation) and rubbish disposal. • An Archaeological Heritage Survey across M74/245 identified five archaeological features, two ethnographic features and an additional 35 isolated finds. Following submission to the Department of Planning, Lands and Heritage ("DPLH") for assessment, the Munglinup River (Site ID 37695), Mungan Wilgie Koort (Site ID 37631) and Munglinup Standing Stone (Site ID 37798) were registered as an Aboriginal Site (Applied Archaeology Australia 2018). • The two ethnographic features lie outside of the required Munglinup development envelope. • A section 18 application was submitted to the ACMC and subsequently granted to enable development of the project in areas registered as Aboriginal sites. • The Munglinup graphite deposit is located within the Shire of Esperance, a predominantly rural area with a population of 14,242 residents. The closest town to the Project is Munglinup, which is 4km to the south. Esperance is the main town and administrative centre for the region, located approximately 105km to the east. • Whilst the Munglinup operations will be new, the local community is generally

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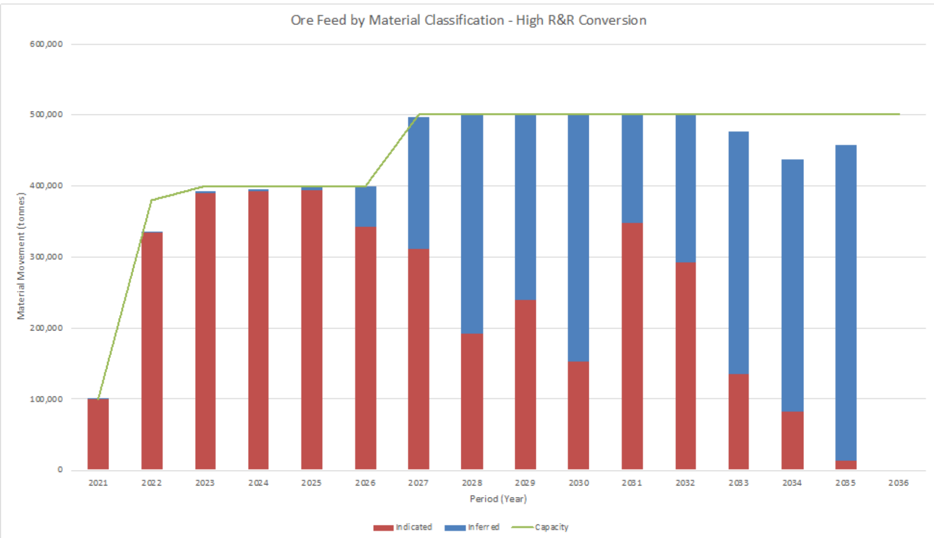
Criteria	Commentary
	familiar with the characteristics of mining, processing and product transport, as other resource extraction operations occur within the shire. Stakeholder consultation conducted to date has identified that the majority of the community are supportive of the Project. During the public consultation period for the Project referral, four submissions where received, suggesting that the community is not concerned about the Project.
Other	• The Company is currently undergoing review of the environmental impact submission by the EPA and EPBC under an accredited process to gain an environmental operating permit. • As there is a Mining Lease in place, no economic evaluation or justification is required.
Classification	• The current Mineral Resource classifies all mineralisation at Munglinup as Indicated and Inferred only. • Given predominantly the proposed mining rate and uncertainty of mineralisation at the local scale, no measured material has been defined under the JORC guidelines. • Currently, 100% of the Ore Reserve has been derived from Indicated Mineral Resources. • A comprehensive resource development and grade control drilling program has been developed and is planned for execution upon granting of project environmental permits. • Pit optimisations and the proposed mining schedule are cognisant of the Mineral Resource classification. • The first 6 years of ore feed is almost entirely classified as probable with the current schedule, including inferred material as "In-Pit Resources" in later years of production. The inferred material will be upgraded to indicated or measured prior to the third year of production.



Criteria	Commentary
Audits or reviews	• Only internal reviews of the Ore Reserve methodology and estimates have been done. • Metallurgical and process design has been reviewed by Orway Mineral Consultants. • Capital and operating costs were reviewed by Lycopodium and Monadelphous

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Criteria	Commentary
	personnel prior to approval by Mondium.
Discussion of relative accuracy/ confidence	• A degree of uncertainty is associated with the Geological and Mineral Resource estimates and the Ore Reserve classification also reflects the level of confidence in the Mineral Resources. The Mineral Resource model is an implicit model that has been translated to a conventional, regularised block model for optimisation and mine planning purposes. Any conversion of this type of a geological model will introduce minor inconsistencies due to the change estimation and reporting methodology. At all stages the model was reconciled back to the previous model to ensure any variability was understood and acceptable. • The design, schedule and financial model on which the Ore Reserves are based has been completed to a Definitive Feasibility Study standard with a corresponding level of confidence (+15%/-5%). • There is a degree of uncertainty regarding estimates of material hardness at depth, geotechnical rock mass characterisation and mineralisation at the local scale. This has been accounted for in the Mineral Resource and subsequent Ore Reserve material categorisation. The Competent Person is satisfied that a suitable margin exists that the Ore Reserve estimate would remain economically viable with any negative impacts applied to these factors or parameters. • There is a degree of uncertainty in the commodity price used, however the Competent Person is satisfied that the assumptions used to determine the economic viability of the Ore Reserves are based on reasonable current data.